

Université d'Ottawa | University of Ottawa

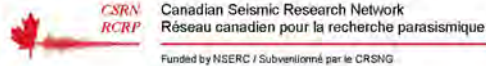
Screening of Buildings for Seismic Considerations

Screening Tool Based on 2005 and 2010 NBCC

Dr. M. Saatcioglu and Dr. M. Shooshtari
Department of Civil Engineering
University of Ottawa



Dr. Simon Foo
Real Property Branch
Public Works and Government Services Canada



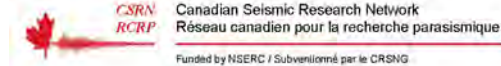
NRC-Seismic Screening Manual for Buildings in Canada

- ❑ NRC developed the Canadian seismic screening manual in 1992 by modifying the ATC-21 document dated 1989.
- ❑ It was adopted to the Canadian seismicity and building practices on the basis of the NBCC-1990.
- ❑ It was further modified to include the inspection of buildings not only from outside (walk down survey), but also from inside, as well as the inspection of drawings.



NRC-Seismic Screening Manual for Buildings in Canada

- ❑ The method used in the Screening Manual is based on the computation of seismic priority index as the product of factors that affect building performance during earthquakes.
- ❑ These factors are related to the seismic requirements of the NBCC-1990, which reflect the Canadian seismicity incorporated into the NBCC-1985. The 1985 seismic hazard map was expressed in terms of Seismic Zones



Seismic Priority Index

Structural Index, SI:

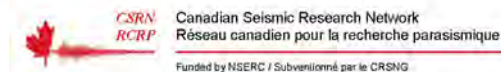
$$SI = A * B * C * D * E$$

Non-Structural Index, NSI:

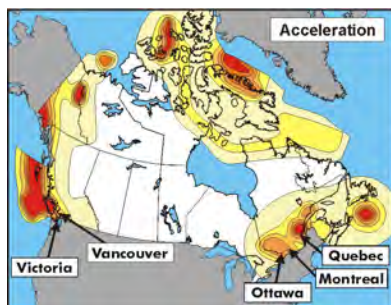
$$NSI = B * E * F$$

Seismic Priority Index, SPI:

$$SPI = SI + NSI$$

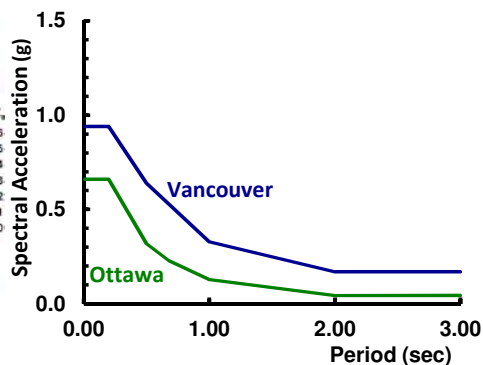


Seismic Hazard

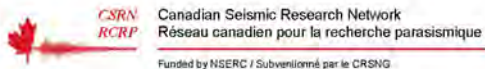


Hazard Map by GSC

In 1990 NBCC, hazard is expressed in terms of Seismic Zones



In 2005 and 2010 NBCC, hazard is expressed in terms of UHS



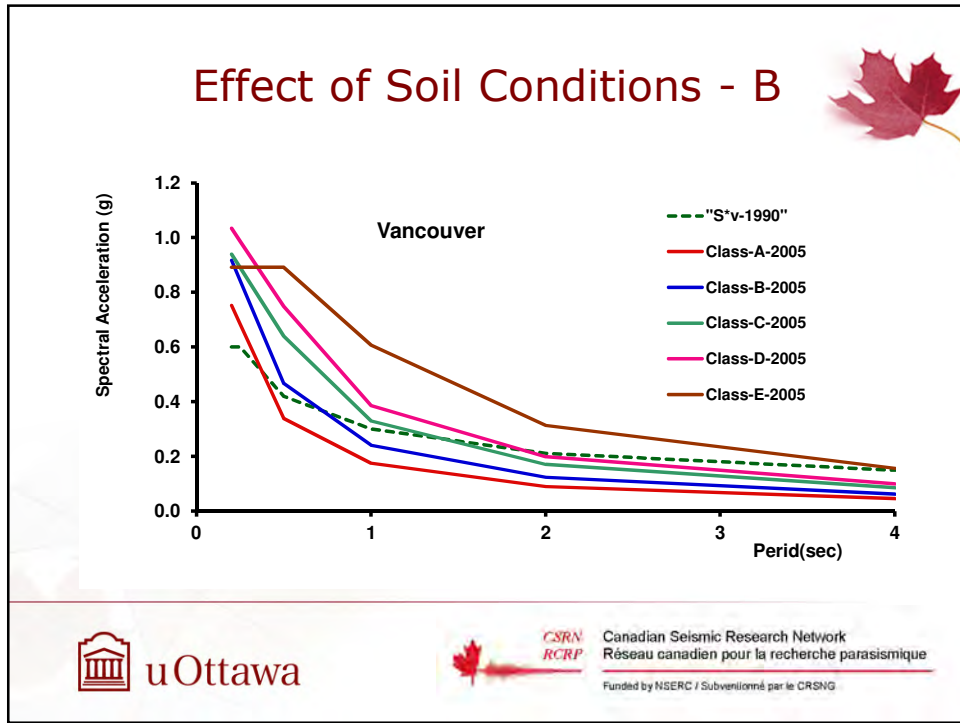
Seismicity Index - A

Province : Ontario City : Ottawa	NBC-95		NBC-2005	
	Z _a = 4	Z _v = 2	S _a (0.2) = 0.66	S _a (0.5) = 0.32
	v = 0.10		S _a (1.0) = 0.13	S _a (2.0) = 0.044

Period(sec)	Frame Category	Seismicity (A) Design NBC			
		Pre-65	65-84	85-05	Post-05
T _a ≤ 1.0	All Frame	2.3	1.5	1.5	1.0
1.0 < T _a < 2.0	All Frame	1.3	0.9	0.9	1.0
2.0 ≤ T _a	MRF	0.6	0.4	0.4	1.0
	BRF	0.8	0.5	0.5	1.0
	SWF	1.3	0.9	0.9	1.0

For buildings with T ≤ 0.5 sec designed prior to 2005, Factor A may be multiplied by 2/3 if the building has some ductility (R_d >= 1.5 as per NBCC-2005).







Effect of Soil Conditions - B

NBCC-2005		NBCC-1990	
Site Class	Soil Profile Name	Categories	Type and Depth of Soil*
A	Hard Rock	1	Rock, dense and very dense coarse-grained soils, less than 15 m deep
B	Rock		
C	Very Dense Soil and Soft Rock	2	Compact coarse-grained soils, less than 15 mm deep.
D	Stiff Soil	3	Very loose and loose coarse grained soils greater than 15 m in depth
E	Soft Soil	4	Very soft and soft fine-grained soils greater than 15 m in depth.

$$B_{(65-05)} = B_{(Post65)} \frac{R_a \text{ or } R_v}{F_{(1990)}}$$





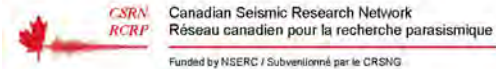
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Effect of Soil Conditions - B (Ottawa)



Soil Conditions (B)		Design NBC			
Period(sec)	Soil	Pre-65	65-84	85-05	Post-05
	Category				
Ta <= 0.2	Class A	0.8	0.8	0.8	1.0
	Class B	0.9	0.9	0.9	1.0
	Class C	1.0	0.8	0.8	1.0
	Class D	1.1	0.8	0.8	1.0
	Class E	1.2	0.9	0.9	1.5
Ta = 0.5	Class A	0.5	0.5	0.5	1.0
	Class B	0.6	0.6	0.6	1.0
	Class C	1.0	0.8	0.8	1.0
	Class D	1.4	0.9	0.9	1.0
	Class E	2.1	1.6	1.6	1.5
1.0 <= Ta	Class A	0.5	0.5	0.5	1.0
	Class B	0.6	0.6	0.6	1.0
	Class C	1.0	0.8	0.8	1.0
	Class D	1.4	0.9	0.9	1.0
	Class E	2.1	1.6	1.6	1.5

For all other soils, site-specific evaluation is required.



Condominium in Concepcion



Shear wall detailing



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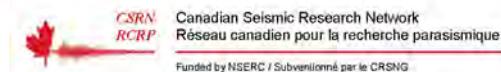
Splice Failure

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Type of Structure - C

- ❑ Factor for Type of Structure reflects the toughness of the structure. A low value indicates the structure has sufficient strength and deformability to absorb seismic induced energy.
- ❑ Inelastic deformability was reflected in earlier codes through coefficient K and then by coefficient R.
- ❑ NBCC-2005/2010 uses $R_d R_o$ product to reduce elastic force levels in exchange of seismic design and detailing of individual elements. This product can be perceived to be approximately equal to the R/U used in NBCC-1990.

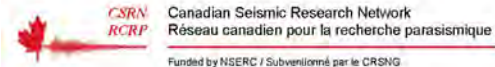
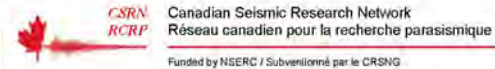


Type of Structure - C



- R_d and R_o values corresponding to full ductility, moderate ductility and conventional construction were used when $S_a(0.2) > 0.75$; $0.2 \leq S_a(0.2) \leq 0.75$ and $S_a(0.2) < 0.2$, respectively.

Type of Structure (C) (For construction type and abbreviations please see Help)														
Design	Wood		Steel				Concrete		Precast		Masonry(Infill)		Masonry	
NBC	WLF-WPB		SLF-SMF-SBF-SCW				CMF-CSW		PCF-PCW		SIW-CIW	IRML-RMC-URM		
Pre-70	1.4	1.6	1.0	1.6	2.0	2.0	2.5	2.0	4.3	3.4	3.3	2.8	3.5	
70-BM	1.4	1.6	1.0	1.6	2.0	1.5	1.5	1.5	3.1	2.6	2.2	1.7	3.5	
BM-05	1.2	1.3	1.0	1.3	1.3	1.0	1.0	1.0	1.7	1.7	1.1	1.1	***	
Post-05	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	***	





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Building Irregularities - D



- ❑ Vertical Irregularities
- ❑ Horizontal Irregularities
- ❑ Short Concrete Columns
- ❑ Soft Storey
- ❑ Pounding
- ❑ Modification
- ❑ Deterioration

Building Irregularities (D)
(D = product of applicable irregularity factors; not to exceed 4.0)

Design NBC	Vertical	Horizontal	Short Concret Columns	Soft-Storey	Pounding	Modification	Deterioration	None
Pre-70	1.3	1.5	1.5	2.0	1.3	1.3	1.3	1.0
Post-70	1.3	1.5	1.5	1.5	1.3	1.0	1.3	1.0



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Building Importance - E



Post Disaster

Special Operational Req.

Others

N = Occupied Area x Occupancy Density x Duration Factor

- Low occupancy: $N < 10$
- Normal occupancy: $N = 10$ to 300
- School or high occupancy: $N = 301 - 3000$
- Post disaster or very high occupancy: $N > 3000$
- Special operational requirements



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Building Importance - E



Parameters of "N"

Primary Use	Occupancy Density (persons/m ²)	Average Weekly Hours of Human Occupancy
Assembly	1	5 – 50
Mercantile, Personal service	0.2	50 – 80
Offices, Institutional, Manufacturing	0.1	50 – 60
Residential	0.05	100
Storage	0.01 – 0.02	100

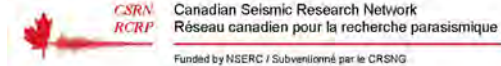


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Building Importance - E



Building Importance (E)					
(For computation of N in the Table, please see Help)					
Design	Low Occupancy N < 10	Normal Occupancy N=10 - 300	High Occupancy N = 301 - 3000	Post Disaster, or Very High Occup.	Special Operational Requirements
NBC					
Pre-70	0.7	1.0	1.5	2.0	3.0
Post-70	0.7	1.0	1.2	1.5	2.0



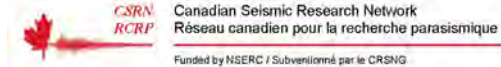
Non-Structural Hazard - F



- Falling hazards
- Hazards to vital operations

Non-Structural Hazards (F) (F= Max (F1,F2))						
			None	Yes	Yes*	
F1	Falling Hazards to Life	Pre-70 NBC	1.0	3.0	6.0	
		Post-70 NBC	1.0	2.0	3.0	
F2	Hazards to Vital Operations	Any Year	1.0	3.0	6.0	

* Only if one or more of the following types of structure and/or building irregularity apply. SMF, CMF, Soft-Storey, Horizontal Irregularity



Province: Ontario City: Ottawa	NBC 95 $Z_a = 4$ $Z_v = 2$ $v = 0.10$	NBC-2005 $S_a(0.2) = 0.66$ $S_a(0.5) = 0.32$ $S_a(1.0) = 0.13$ $S_a(2.0) = 0.044$
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Period(sec)	Frame Category	Design NBC			
		Pre-65	65-84	85-05	Post-05
$T_a \leq 1.0$	All Frame	2.3	1.5	1.5	1.0
$1.0 < T_a < 2.0$	All Frame	1.3	0.9	0.9	1.0
	MRF	0.6	0.4	0.4	1.0
$2.0 \leq T_a$	BRF	0.8	0.5	0.5	1.0
	SWF	1.3	0.9	0.9	1.0

For buildings with $T < 0.5$ sec designed prior to 2005, Factor A may be multiplied by 2/3 if the building has some ductility ($R_d > 1.5$ as per NBCC-2005).

Period(sec)	Soil Category	Design NBC			
		Pre-65	65-84	85-05	Post-05
$T_a \leq 0.2$	Class A	0.8	0.8	0.8	1.0
	Class B	0.9	0.9	0.9	1.0
	Class C	1.0	0.8	0.8	1.0
	Class D	1.1	0.8	0.8	1.0
	Class E	1.2	0.9	0.9	1.5
$T_a = 0.5$	Class A	0.5	0.5	0.5	1.0
	Class B	0.6	0.6	0.6	1.0
	Class C	1.0	0.8	0.8	1.0
	Class D	1.4	0.9	0.9	1.0
	Class E	2.1	1.6	1.6	1.5
$1.0 < T_a$	Class A	0.5	0.5	0.5	1.0
	Class B	0.6	0.6	0.6	1.0
	Class C	1.0	0.8	0.8	1.0
	Class D	1.4	0.9	0.9	1.0
	Class E	2.1	1.6	1.6	1.5

For all other soils, site-specific evaluation is required.

Design	Type of Structure (C) (For construction type and abbreviations please see Help)							
	Wood	Steel			Concrete	Precast	Masonry(Infill)	Masonry
NBC	WLF-WFB	SLF-SMF-SBF-SCW	CMF-CSW	PCF-PCW	SIW-CIW	IRML-RMC-URM		
Pre-70	1.4 1.6	1.0 1.6 2.0 2.0	2.5 2.0	4.3 3.4	3.3	2.8 3.5		
70-84	1.4 1.6	1.0 1.6 2.0 1.5	1.5 1.5	3.1 2.6	2.2	1.7 3.5		
85-05	1.2 1.3	1.0 1.3 1.3 1.0	1.0 1.0	1.7 1.7	1.1	1.1 ---		
Post-05	1.0 1.0	1.0 1.0 1.0 1.0	1.0 1.0	1.0 1.0	1.0	1.0 ---		

Design	Building Irregularities (D) (D = product of applicable irregularity factors; not to exceed 4.0)							
	Vertical	Horizontal	Short Concrete Columns	Soft-Storey	Pounding	Modification	Deterioration	None
Pre-70	1.3	1.5	1.5	2.0	1.3	1.3	1.3	1.0
Post-70	1.3	1.5	1.5	1.5	1.3	1.0	1.3	1.0

Design	Building Importance (E) (For computation of N in the Table, please see Help)				
	Low Occupancy N < 10	Normal Occupancy N=10-300	High Occupancy N = 301-3000	Post Disaster, or Very High Occup. N > 3000	Special Operational Requirements
Pre-70	0.7	1.0	1.5	2.0	3.0
Post-70	0.7	1.0	1.2	1.5	2.0

F1	F2	Non-Structural Hazards (F) (F = Max (F1,F2))		
		None	Yes	Yes*
Falling Hazards to Life	Pre-70 NBC Post-70 NBC	1.0 1.0	3.0 2.0	6.0 3.0
Hazards to Vital Operations	Any Year	1.0	3.0	6.0

* Only if one or more of the following types of structure and/or building irregularity apply.
SMF, CMF, Soft-Storey, Horizontal Irregularity

Structural Index (SI) $SI = A \times B \times C \times D \times E$
Seismic Priority Index (SIP) $SIP = SI + NSI$
Non-Structural Index (NSI) $NSI = B \times E \times F$

Print on File Continue Help

Province: Ontario
City: Ottawa
Project Name: Sample Building

Design NBC: Pre-65
Frame Category: MRF
Soil Category: Class D

Calculate Fundamental Period
Enter Fundamental Period (sec): 1.2

Type of Structure:
 Wood (WLF, WFB)
 Concrete (CMF, CSW)
 Steel (SLF, SMF, SBF, SCW)
 Precast (PCF, PCW)
 Masonry Infill (SIW, CIW)
 Masonry (RML, RMC, URM)

Building Irregularities:
 Vertical Pounding
 Horizontal Modification
 Short Concrete Columns Deterioration
 Soft Storey None

Building Importance:
 Please select only one of the three categories:
 Post-disaster Building Special Operational Requirements Other Buildings
 If "Other Buildings" is selected, enter occupancy information below:
 Occupied Area (meter square):
 Occupancy Density (Persons/meter square):
 Average Weekly Hours of Human Occupancy (Maximum 100):

Non-Structural Hazards:
 Falling Hazards to Life: Yes None
 Hazards to Vital Operations: Yes None

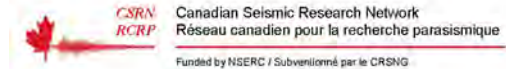
To See The Results, Click Here

Results			
A = 1.300	D = 4.000	SI = A x B x C x D x E =	35.620
B = 1.370	E = 2.000	NSI = B x E x F =	16.440
C = 2.500	F = 6.000	SIP = SI + NSI =	52.060

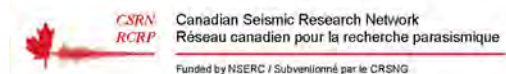
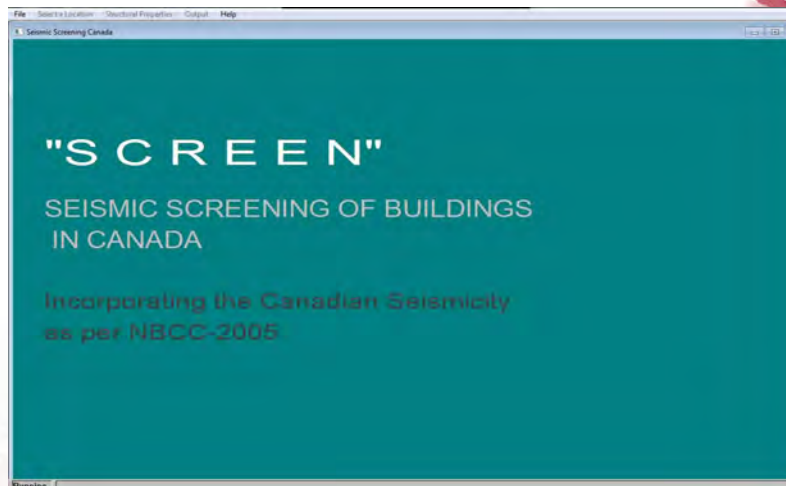
Help Proceed with the Next Building Close

Ranking of Screening Indices

- ❑ Higher scores in screening indices indicate higher priority for further evaluation
- ❑ It is difficult to define the level of “acceptable score”
- ❑ SI or NSI score of 1.0 to 2.0 indicate compliance with NBCC-2005 and NBCC-2010
- ❑ $SPI < 10$ indicates low priority
- ❑ SPI of 10 to 20 indicates medium priority
- ❑ $SPI > 20$ indicates high priority
- ❑ $SPI > 30$ can be considered potentially hazardous



EXAMPLES AND USE OF “SCREEN”



Seismic Risk Assessment of Concrete Structures in Ottawa

Dr. M. Saatcioglu, Civil Engineering, uOttawa

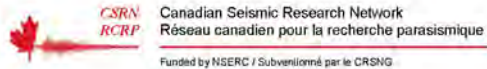
Dr. S. Tesfamariam, Civil Engineering, UBC

Dr. M. Sawada, Geography, uOttawa

Ms. Kate Ploeger, Geography, uOttawa

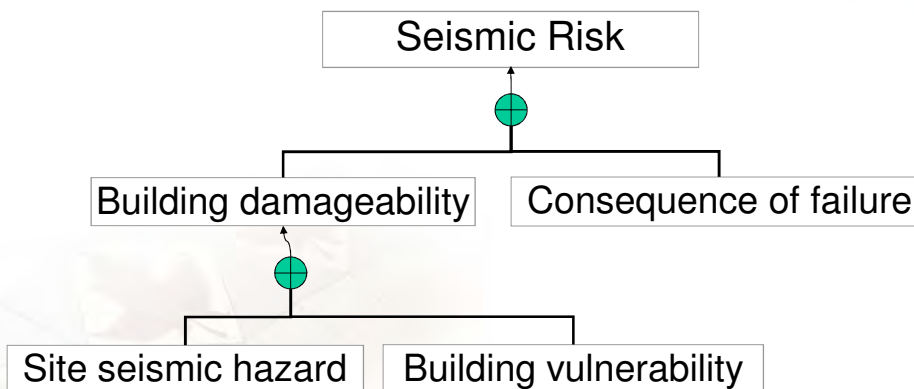
Mr. Amid Elsabbagh, Civil Engineering, uOttawa

Mr. Erik Selin, Mathematics/Computer Science, uOttawa



Seismic Risk

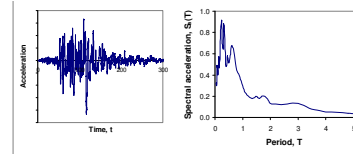
$$\text{Risk} = \text{Building damageability} \times \text{Consequence of failure}$$



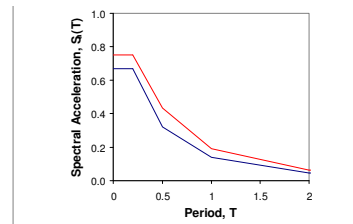
Site Seismic Hazard

- ❑ Canadian seismicity is expressed in the National Building Code of Canada in terms of Uniform Hazard Spectra (UHS)
- ❑ UHS compatible synthetic ground motion records have been generated
- ❑ Soil amplification effects can be considered as per NBCC
- ❑ Seismic microzonation is available for various cities in Canada, including the City of Ottawa, providing the basis for site-specific risk analysis

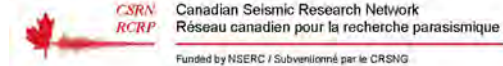
Site specific earthquake record



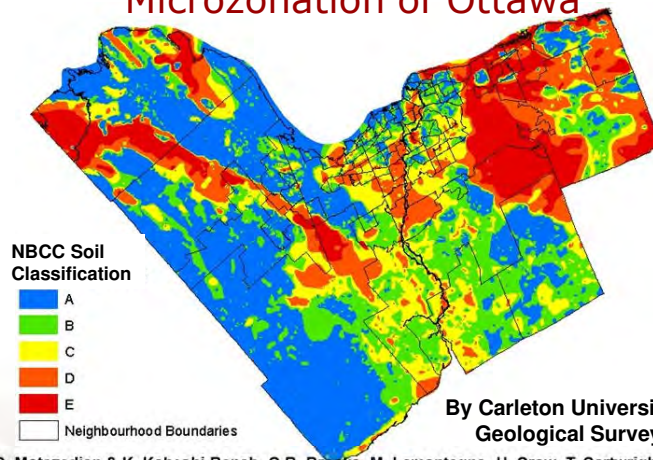
Site specific design response spectrum



Compute spectral acceleration (S_a)



Microzonation of Ottawa



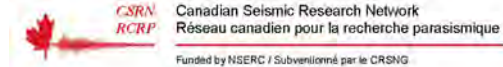
NBCC Soil Classification

- A
- B
- C
- D
- E

Neighbourhood Boundaries

By Carleton University and NRCan,
Geological Survey of Canada

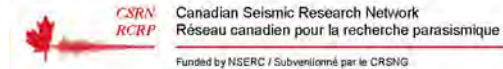
J.A. Hunter, D. Motazedian & K. Kaheshi-Banab, G.R. Brooks, M. Lamontagne, H. Crow, T. Cartwright, A. Pugin, M. Pyne. DATA COLLECTION FOR EARTHQUAKE HAZARD MAPPING IN THE OTTAWA AREA. In : J. Locat, D. Perret, D. Turmel, D. Demers et S. Leroueil, (2008). *Comptes rendus de la 4e Conférence canadienne sur les géorisques: des causes à la gestion. Proceedings of the 4th Canadian Conference on Geohazards : From Causes to Management*. Presse de l'Université Laval, Québec, 594 p. <http://www.gpr.uqam.ca/~gpr/act/4econf/ottawa/ottawatechnologies/murtes.pdf>



Building Vulnerability

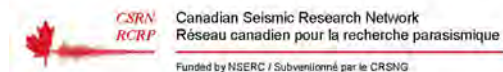
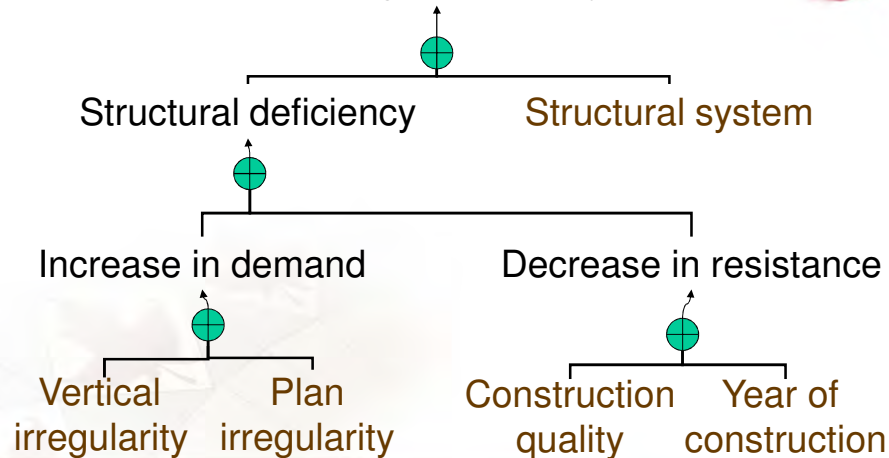
Can be assessed in three different levels of complexity and accuracy:

- ❑ Tier I – Screening based on walk-down survey
- ❑ Tier II – Detailed evaluation using simple computations
- ❑ Tier III – Dynamic Response History Analysis

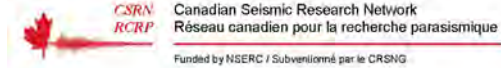
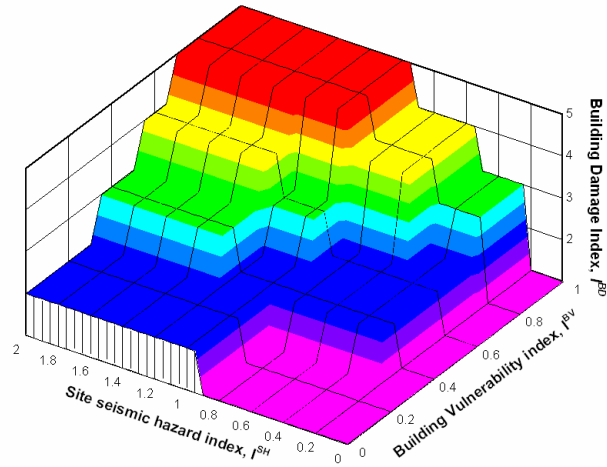


Tier – I Evaluation

Building vulnerability



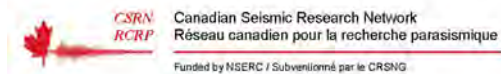
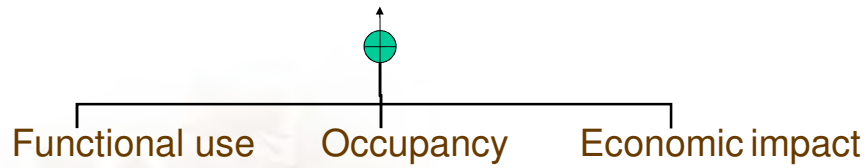
Building Damageability



Consequence of Failure



Building importance/ exposure



Risk Assessment Tool



CanRisk Tier 1 Evaluation

Basic Information | SSH | Damage | Risk

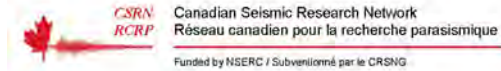
Location and site soil condition
 City: AB - Banff
 Soil type: A

Exposure
 Occupancy: D-10
 Building use: Hotel
 Economic impact: Significant

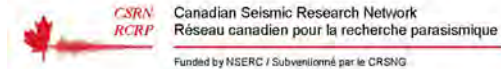
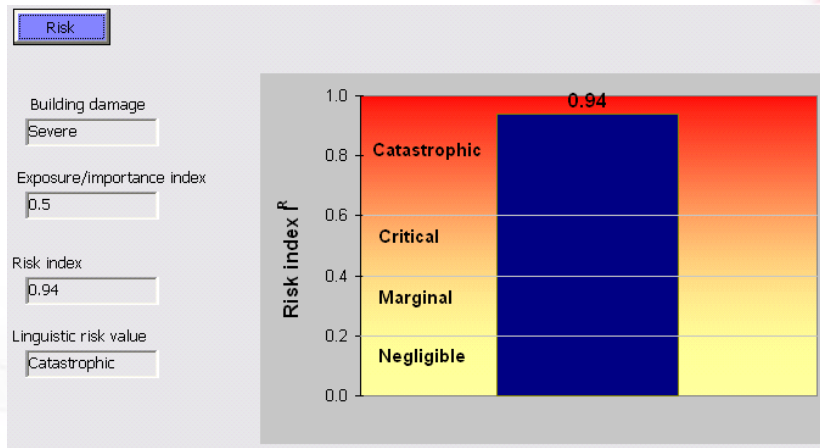
Building related information
 Building type: C1
 Number of stories: 5
 Vertical irregularity: No
 Plan irregularity: No
 Construction quality: Good
 Year of construction: 1959

Concrete Moment Frames

Print




Risk Assessment Tool




Tier – II Evaluation

However, the parameters that contribute to Building Vulnerability are far too complex



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Tier – II Evaluation

```

    graph TD
      BV[Building vulnerability] --> ID[Increase in demand]
      BV --> DR[Decrease in resistance]
      BV --> PA[Problems of adjacency]
      
      ID --> W[Walls]
      ID --> RSJ[Relative strength at joints]
      ID --> VI[Vertical irregularity]
      ID --> PI[Plan irregularity]
      ID --> D[Diaphragm]
      
      W --> SW[Structural walls]
      W --> MW[Masonry walls]
      MW --> R[Reinforced]
      MW --> UR[Unreinforced]
      
      RSJ --> DC[Discontinuous columns]
      
      VI --> SC[Short column]
      VI --> WS[Weak story]
      VI --> SS[Soft story]
      
      PI --> DC2[Diaphragm continuity]
      PI --> REC[Re-entrant corners]
      
      DR --> CQ[Construction quality]
      DR --> YOC[Year of construction]
      DR --> DQ[Design quality]
      
      YOC --> YC[Year of construction]
      YOC --> CE[Code enforcement]
      
      DQ --> C[Columns]
      DQ --> J[Joins]
      DQ --> D[Diaphragms]
      
      PA --> FE[Floor elevation]
      PA --> SBA[Spacing b/n adjacent buildings]
      
      SD[Structural degradation/weakening] --> SPEQ[Subjected to previous EQ]
      SD --> COR[Corrosion]
    
```

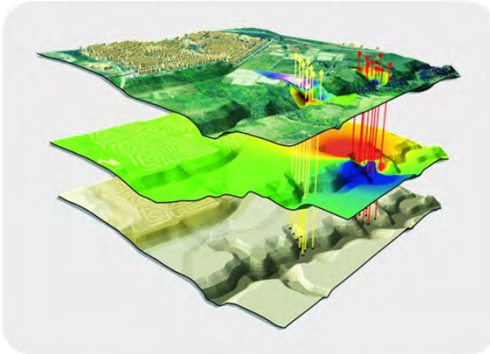


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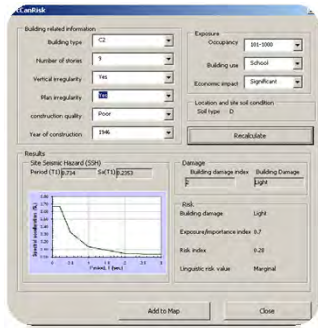
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• arcCanRisk



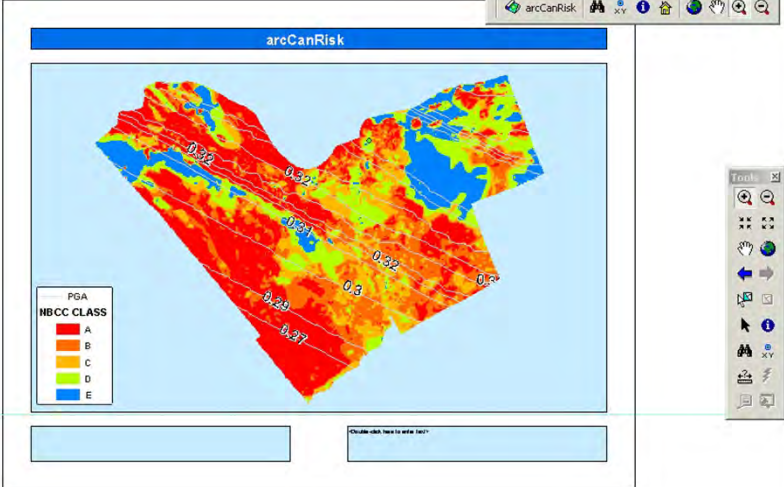








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arcCanRisk







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arcCanRisk – Future directions

- Addition of other structures for assessment
- Incorporation of OFCs
- Incorporation of Tier 3 analysis
- ArcGIS 10 add-on integration
- Web-based analysis
- Area based assessments.
- Incorporation of Social Consequences/Casualties Module
- Incorporation of Economic Consequences Module
- Emergency Response Tool (first 72 hours)



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CanRisk - Welcome!

Home About CanRisk Services Research Contact Us

Selected Position at (45.45803823532799,-75.68414970361323) has soil type A at an estimated shear wave velocity of 1964Vs.

Evaluate Selected Position

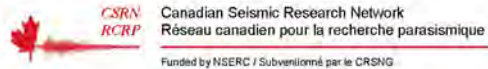
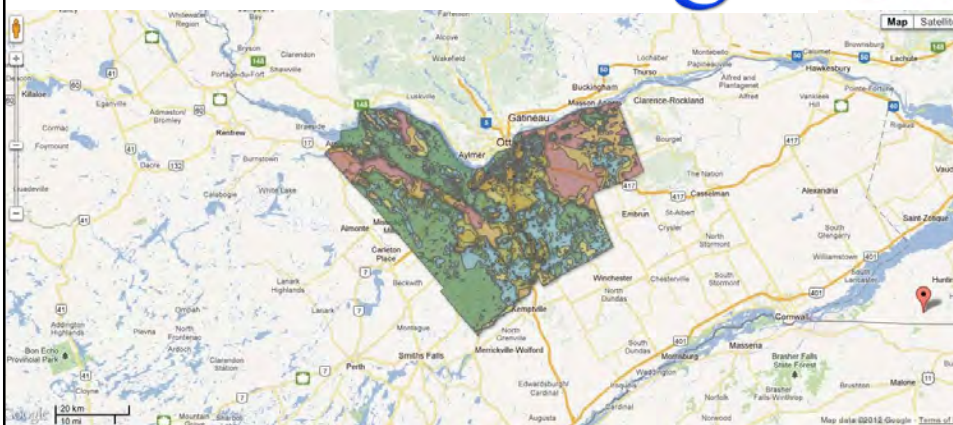
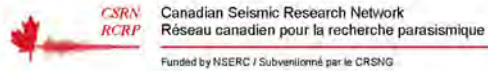
100% 75% 50% 25% Hide

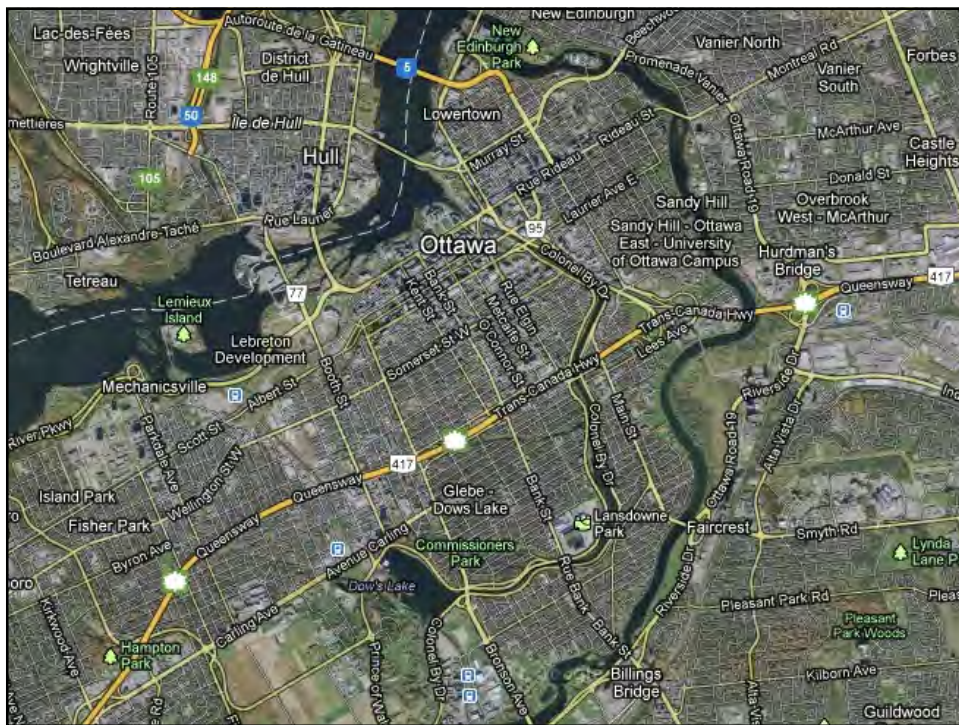
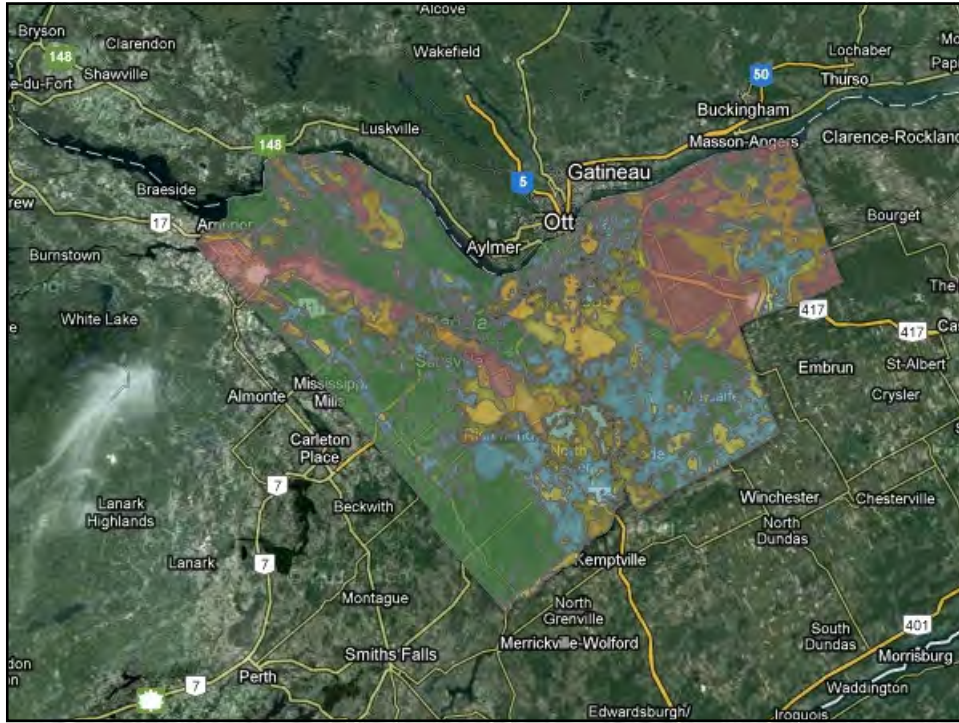
Map Satellite

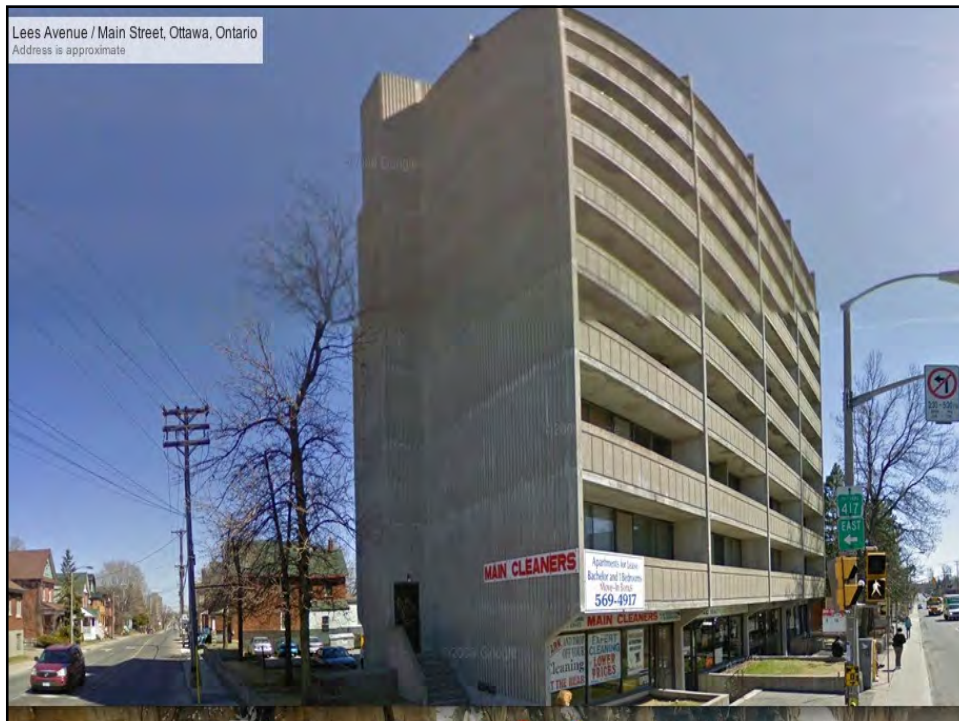
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DEMONSTRATION OF A WEB-BASED SEISMIC RISK ASSESMENT TOOL







Show/Hide Soil Type Building Type **C3** Vertical Irregularity **Yes** Plan Irregularity **Yes** Construction Quality **Average** Year of Construction **1960** Soil Class **D**
 Number of Stories **9** Building Type **Apartment** Occupancy **101-1000** Economic Impact **Average** Username **canrisk** Password *********
 Evaluate

Linguistic Risk Index: Negligible
 Risk Index: 0.13
 Linguistic Damage Index: Light
 Damage Index: 2

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Show/Hide Soil Type Building Type **C3** Vertical Irregularity **Yes** Plan Irregularity **Yes** Construction Quality **Average** Year of Construction **1960** Soil Class **D**
 Number of Stories **1** Building Type **Apartment** Occupancy **101-1000** Economic Impact **Average** Username **canrisk** Password *********
 Evaluate

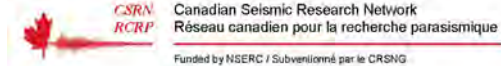
Linguistic Risk Index: Critical
 Risk Index: 0.49
 Linguistic Damage Index: Moderate
 Damage Index: 3

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Data Collection for City of Ottawa



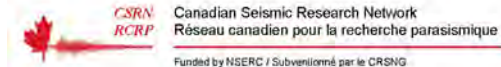
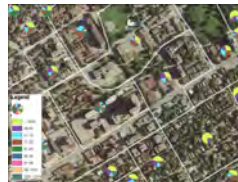
- Google Earth 
- Street view 
- Bing Maps 
- ArcGIS 
- ArcObjects
 - Visual Studio.Net
- Android
 - App Inventor
 - Eclipse Android SDK (Java)
- GIS layers
- Field Data Collection
- Lab Data Collection



Data Collection for City of Ottawa



- Footprints
- Statistics Canada
- Zoning Data



Data Collection – City of Ottawa



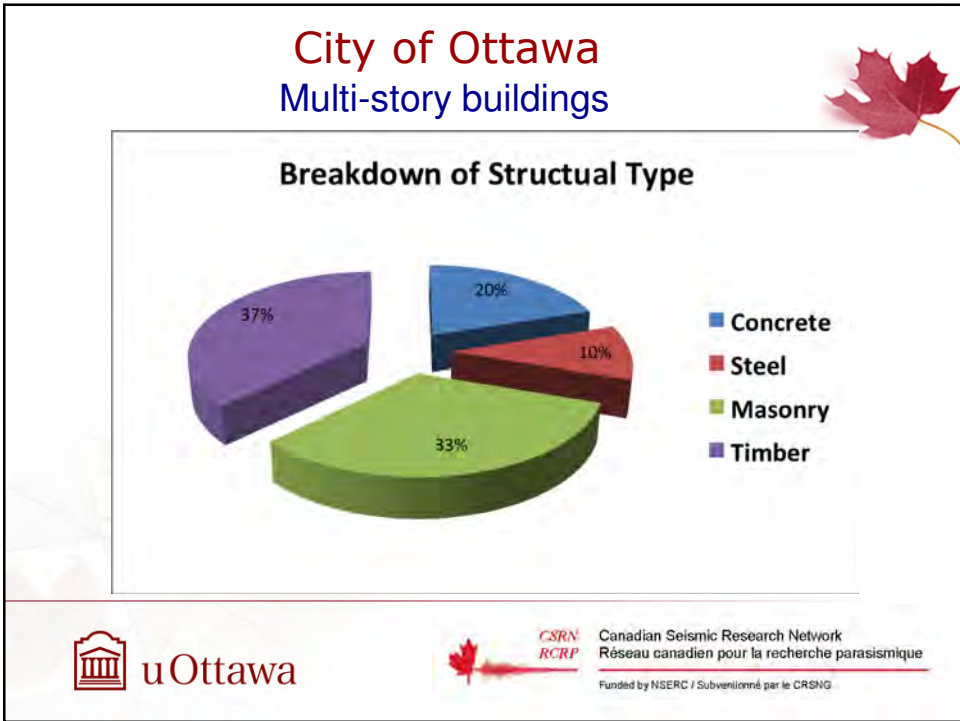
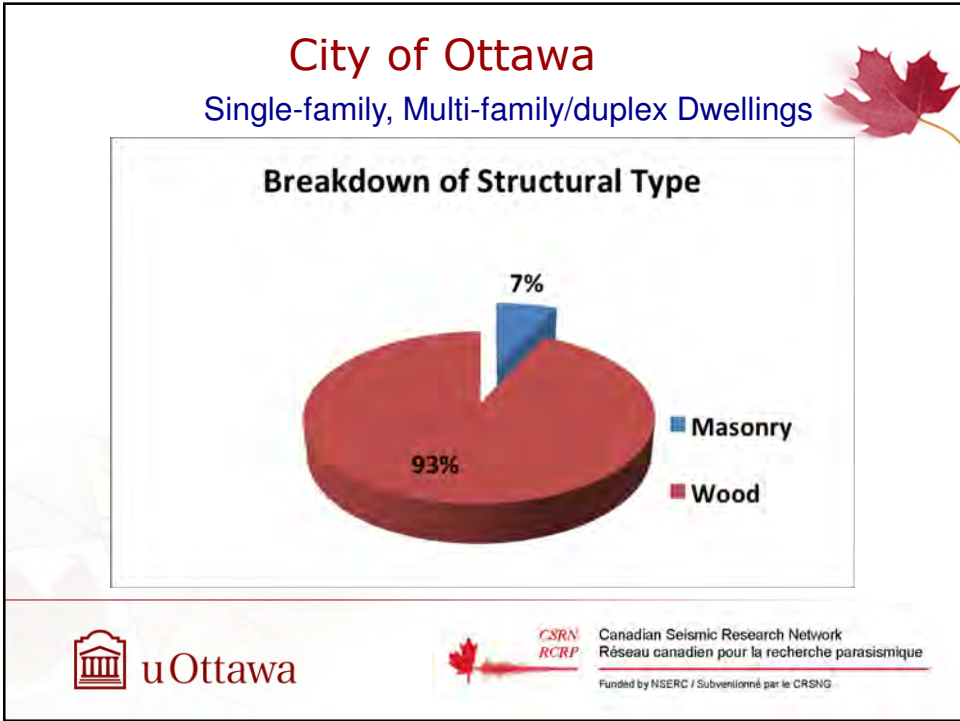
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City of Ottawa

- ❑ A total of 6233 buildings have been surveyed to date.
- ❑ Of this number, 5105 are single family, multi-family/duplex dwellings.
- ❑ The remaining (1128) are multi-story buildings of different use and occupancy categories.



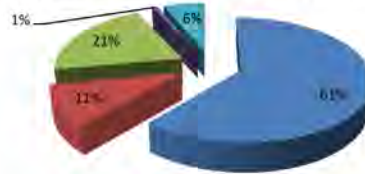
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City of Ottawa

Breakdown of Concrete Construction Type

- Concrete Moment Frame
- Concrete Shear Walls
- Concrete Frame with Unreinforced Masonry Infill Walls
- Precast Concrete Tilt-Up Walls
- Precast Concrete Frames with Concrete Shear Walls



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Thank You....

Questions and Comments?



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